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- [Description](#)
- [Table of Contents](#)

Table of Contents

General lectures

Actual developments in the nonlinear shell theory – state of the art and new applications of the six-parameter shell theory

H. Altenbach & V.A. Eremeyev

Nonlinear vibrations of shells: Experiments, simulations and applications

M. Amabili & F. Alijani

3D-shell mathematical models and finite elements: From mathematical and physical insight to application examples

D. Chapelle

Mechanics design and analyses of stretchable electronics

Y. Zhang, K.C. Hwang & Y. Huang

On geometrically non-linear FEA of laminated FRP composite panels

I. Kreja

Theoretical modelling

An analytical solution to the problem of interaction of a circular plate with an inhomogeneous soft layer

S.M. Aizikovich, A.S. Vasiliev, S.S. Volkov, B.I. Mitrin & E.V. Sadyrin

Laminated smart shell structures; theory and analysis

T.M.B. Albarody & H.H. Al-Kayiem

On the surface vis impressa caused by a fluid-solid contact

J. Badur, P. Ziółkowski, W. Zakrzewski, D. Sławinski, M. Banaszekiewicz, O. Karczmarczyk, S. Kornet & P.J. Ziółkowski

Nonclassical theories for bending analysis of orthotropic circular plate

S. Bauer & E. Voronkova

On the characterization of drilling rotation in the 6-parameter resultant shell theory

M. Bîrsan & P. Neff

Existence of solutions of dynamic contact problems for elastic von Kármán-Donnell shells

I. Bock & J. Jarušek

On the effectiveness of higher-order terms in layer-wise shell models

E. Carrera, A. Lamberti & M. Petrolo

The free material design of thin elastic shells

S. Czarnecki, R. Czubacki, G. Dzierzanowski & T. Lewinski

Moderately large deflections of thin densely ribbed plates

Ł. Domagalski & M. Gajdzicki

Theory of shells as a product of analytical technologies in elastic body mechanics

V. Eliseev & Y. Vetyukov

On effective stiffness of a three-layered plate with a core filled with a capillary fluid

V.A. Eremeyev, E.A. Ivanova, H. Altenbach & N.F. Morozov

General dynamic theory of micropolar elastic orthotropic multilayered thin shells

A.J. Farmanyan & S.H. Sargsyan

Stationary deformation of compound shell structures under arbitrary loadings

Y.M. Grigorenko, E.I. Bespalova & G.P. Urusova

TUBA finite elements: Application to the solution of a nonlinear Kirchhoff-Love shell theory

V. Ivannikov, C. Tiago & P.M. Pimenta

Shell Structures: Theory and Application

[Previous Chapter](#)

[Next Chapter](#)

[Table of Contents](#)



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Chapter 7. Laminated smart shell structures; theory and analysis

T . M . B . Albarodyand H . H . Al-Kayiem

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Laminated smart shell structures; theory and analysis

T.M.B. Albarody & H.H. Al-Kayiem

Universiti Teknologi PETRONAS, Bandar Seri Iskandar, Perak, Malaysia

ABSTRACT: Modeling of shells integrated with smart lamina and taking account of thermo-magneto-electro-elastic fields represents a challenge to be formulated and solved. In the present work, analytical model is proposed based on Hamilton's variational principle linked with Gibbs free energy functions. The model is casted according to the first-order shear deformation shell theory. The exact solution is derived for linearly constitutive properties, simply supported, shallow shell having rectangular plane-form under static loadings. The effects of the material properties, lay-ups of the constituent layers, and shell parameters on the free vibration behavior are investigated and analyzed. The accurate treatment of thermal, magnetic, electric, and elastic energies that are taken into account in this smart shell yields rather sophisticated equations for magnetic inductions, electric displacements and stress resultants. Therefore, the introduced model is expected to provide a foundation to investigate the interactive effects among the thermal, magnetic, electric, and elastic fields in smart shell structures.

1 INTRODUCTION

A smart shell is a thin-walled solid structure integrated with piezoelectric, magnetostrictive and like materials. Smart materials are used to provide new features to shell structures used frequently in construction of spacecrafts and aerospace vehicles. In fact, the idea of developing adaptive structures is to create new properties that can be utilized in health monitoring, aside of the structures designed for load supporting capability.

Several accurate solutions have been found in the literature for multilayered piezoelectric and magnetostrictive plates. Some of them were found for special cases of Pan's analysis. Heyliger (1996) demonstrated the free vibration analysis of the simply supported (SS) and multilayered magneto-electro-elastic (MEE) plates under cylindrical bending. Then, Heyliger (2004a,b) studied two cases of the MEE plates subjected to static fields, one under cylindrical bending only and the other completely traction-free under surface potentials.

In this paper, an analytical model of the smart shell based on the first-order shear deformation (FOSD) theory is presented. We examine mathematically the interactive effects of the thermal, magnetic, electric and elastic fields on the vibration of the smart shell structures.

2 THEORETICAL FORMULATION

2.1 Constitutive Relations

The thermodynamic potential Q of a linear quasi-static and reversible system subjected to mechanical,

electric, magnetic, and thermal influences can be approximated by:

$$2Q = \zeta_{ijkl}^{E,G,T} \varepsilon_{ij} \varepsilon_{kl} - \epsilon_{mnn}^{S,G,T} \zeta_m \zeta_n - \mu_{pq}^{S,E,T} \chi_p \chi_q - \theta^{S,E,G} \tau^2 - 2\varrho_{mkl}^{G,T} \varepsilon_{kl} \zeta_m - 2\kappa_{pkl}^{E,T} \varepsilon_{kl} \chi_p - 2\lambda_{kl}^{E,G} \varepsilon_{kl} \tau - 2\eta_{pn}^{S,T} \zeta_n \chi_p - 2\rho_n^{S,G} \zeta_n \tau - 2\gamma_q^{S,E} \chi_q \tau, \quad (1)$$

where Q is known as the Gibbs free energy. The constitutive relations are expressed formally as:

$$\begin{aligned} S_{ij} &= \left(\frac{\partial Q}{\partial \varepsilon_{ij}} \right) = [\zeta_{ijkl}^{E,G,T} \varepsilon_{ij} - \varrho_{mkl}^{G,T} \zeta_m - \kappa_{pkl}^{E,T} \chi_p - \lambda_{kl}^{E,G} \tau], \\ E_k &= - \left(\frac{\partial Q}{\partial \zeta_n} \right) = [\varrho_{ijn}^{G,T} \varepsilon_{ij} + \epsilon_{mnn}^{S,G,T} \zeta_m + \eta_{pn}^{S,T} \chi_p + \rho_n^{S,G} \tau], \\ G_l &= - \left(\frac{\partial Q}{\partial \chi_q} \right) = [\kappa_{ijq}^{E,T} \varepsilon_{ij} + \eta_{mq}^{S,T} \zeta_m + \mu_{pq}^{S,E,T} \chi_p + \gamma_q^{S,E} \tau], \\ T &= - \left(\frac{\partial Q}{\partial \tau} \right) = [\lambda_{ij}^{E,G} \varepsilon_{ij} + \rho_m^{S,G} \zeta_m + \gamma_p^{S,E} \chi_p + \theta^{S,E,G} \tau]. \end{aligned} \quad (2)$$

2.2 Kinematic relations

According to the FOSD shell theory, the following representation of the 3D displacement, electric and magnetic potentials is postulated:

$$\begin{aligned} u(\alpha, \beta, \zeta, t) &= u_o(\alpha, \beta, t) + \zeta \psi_\alpha(\alpha, \beta, t), \\ v(\alpha, \beta, \zeta, t) &= v_o(\alpha, \beta, t) + \zeta \psi_\beta(\alpha, \beta, t), \\ w(\alpha, \beta, \zeta, t) &= w_o(\alpha, \beta, t), \\ \vartheta(\alpha, \beta, \zeta, t) &= -(\vartheta_o(\alpha, \beta, t) + \zeta \vartheta_1(\alpha, \beta, t)), \\ \varphi(\alpha, \beta, \zeta, t) &= -(\varphi_o(\alpha, \beta, t) + \zeta \varphi_1(\alpha, \beta, t)), \end{aligned} \quad (3)$$

